

Parametrization

- Surfaces: $S = r(x, y) = \langle x, y, f(x, y) \rangle$ where $(x, y) \in D$

Ex: $x^2 + y^2 = 2$, $z \leq 9 \rightarrow r(b, \theta) = \langle \sqrt{b} \cos \theta, \sqrt{b} \sin \theta, b \rangle$,
where: $0 \leq b \leq 9$, $0 \leq \theta \leq 2\pi$

$$r(x, y) = \langle x, y, x^2 + y^2 \rangle, \text{ where } (x, y) \in D, D: \{x^2 + y^2 \leq 3\}$$

- Curves

- Circle: $x^2 + y^2 = a^2$; $r(t) = \langle a \cos t, a \sin t \rangle$; $0 \leq t \leq 2\pi$

Ex: $(x-1)^2 + y^2 = 1$; $r(t) = \langle \cos t + 1, \sin t \rangle$; $0 \leq t \leq 2\pi$

- Ellipse: Separate y radius and x radius

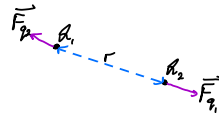
$$r(t) = \langle a \cos t, b \sin t \rangle; 0 \leq t \leq 2\pi$$

- Cylinder Helix: $r(t) = \langle a \cos t, a \sin t, \frac{bt}{2\pi} \rangle$; where b is period length of helix

Coulomb's Law

$$F_q = \frac{q_1 q_2}{4\pi \epsilon_0 \cdot r^2}$$

Electric Permittivity
in Vacuum: $\frac{1}{36\pi} \epsilon = 9 \frac{C}{m^2}$

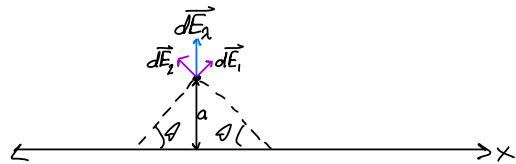


- Permittivity: physical quantity describing how an electric field responds to a dielectric medium
- Electric Field at any point created by Q :

$$E_q = \frac{Q}{4\pi \epsilon_0 \cdot r^2}$$

- Line of Charge ($\lambda = Q/x$):

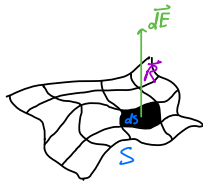
$$E_\lambda = \frac{\lambda}{2\pi \epsilon_0 a}$$



- Plane of Charge ($\sigma = Q/y$)

$$E_\sigma = \frac{\sigma}{2\epsilon_0}$$

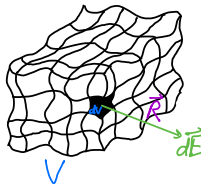
- Surface of Charge ($\sigma = Q/A$)



$$d\vec{E} = \frac{1}{4\pi\epsilon_0} \cdot \frac{dQ}{|\vec{R}|^2} \cdot \hat{R}, \quad dQ = \sigma dS$$

$$\vec{E} = \frac{\sigma}{4\pi\epsilon_0} \int_S \frac{dS}{|\vec{R}|^3} \cdot \vec{R}$$

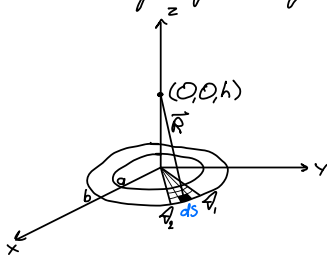
- Volume of Charge ($\rho = Q/V$)



$$d\vec{E} = \frac{1}{4\pi\epsilon_0} \cdot \frac{dQ}{|\vec{R}|^2} \cdot \hat{R}, \quad dQ = \rho dV$$

$$\vec{E} = \frac{\rho}{4\pi\epsilon_0} \int_V \frac{dV}{|\vec{R}|^3} \cdot \vec{R}$$

- Rings of Charge



$$dS = r dr d\theta$$

$$d\vec{E} = \frac{1}{4\pi\epsilon_0} \cdot \frac{dQ}{r^2 + h^2} \cdot \hat{R}, \quad dQ = \sigma dS = \sigma r dr d\theta$$

$$\vec{E} = \frac{\sigma}{4\pi\epsilon_0} \int_S \frac{r}{(r^2 + h^2)^{3/2}} \cdot \vec{R} dr d\theta = \frac{\sigma \cdot h}{4\pi\epsilon_0} \int_0^{2\pi} \int_0^b \frac{r}{(r^2 + h^2)^{3/2}} \cdot dr d\theta \cdot \hat{k}$$

Work

$$dW = -q \vec{E} \cdot d\vec{r} \longrightarrow W = -q \int_{\text{initial}}^{\text{final}} \vec{E} \cdot d\vec{r} \text{ Joules}$$

final/initial is the distance between charges

- Adding work to system: $W > 0$
- Removing work from system: $W < 0$

$$dW_c = |\vec{F}_c| \cdot ds$$

$$\begin{aligned} &\longrightarrow \text{force along path "C"} \longrightarrow "L(t)" \text{ is parametrized "C"} \\ &= \vec{F}(L(t)) \cdot \frac{d\vec{L}}{dt} \longrightarrow W_c = \int_{t_i}^{t_f} \vec{F}(L(t)) \cdot \frac{d\vec{L}}{dt} dt \end{aligned}$$

Potential

$$V_{\text{final}} - V_{\text{initial}} = - \int_{\text{initial}}^{\text{final}} \vec{E} \cdot d\vec{r} \text{ Volts}$$

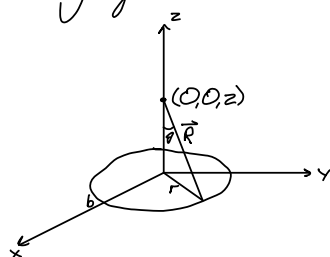
- ΔV is positive if work moves charges closer

• Static Electric Field

- A **conservative** field; path independent

$$\oint \vec{E} \cdot d\vec{r} = 0 \rightarrow \text{Kirchoff's Voltage Law for closed loop}$$

• Ring of Potential



$$\vec{E}(z) = \frac{Qz}{4\pi\epsilon_0(r^2+z^2)^{3/2}} \cdot \hat{k} \quad \frac{N}{m}$$

$$V = - \int_{\infty}^z \vec{E} \cdot d\vec{r} = - \int_{\infty}^z \frac{Qz}{4\pi\epsilon_0(r^2+z^2)^{3/2}} \cdot \hat{k} \cdot d\vec{r} \cdot \hat{k}$$

$$= \frac{Q}{4\pi\epsilon_0\sqrt{r^2+z^2}} \quad \text{Volts}$$

• difference in voltage between point of interest, and infinity

Line Integral

- The line integral of a vector field $\vec{F}(x,y,z)$ on a curve $C: \vec{r}(t)$ is defined by:

$$\int_C \vec{F} \cdot d\vec{r} = \int_a^b \vec{F}(\vec{r}(t)) \cdot \vec{r}'(t) dt =$$

Gradient Fields

- Electric field created by a charge distribution is a gradient field
- There exists a scalar function V such that:

$$\vec{E} = -\vec{\nabla} V$$

$$\langle E_x, E_y, E_z \rangle = -\langle \frac{\partial V}{\partial x}, \frac{\partial V}{\partial y}, \frac{\partial V}{\partial z} \rangle$$

- To solve for V , determine all **terms** that could be excluded by partial:

$$V = \int E_x dx + C(y,z)$$

- Work done by a gradient field does not depend on path
- If $\vec{G} = \vec{\nabla} g \rightarrow$ the second partial derivatives are equal, then the **Curl** equals 0
- If $\vec{\nabla} \times \vec{G} \neq 0$; then $\vec{G}$ is not a gradient field, otherwise $\vec{G}$ could be a gradient field
- **Curl** is related to rotation of gradient field

Gauss' Law

- Electric Flux Density ($\vec{D}$)

$$\Phi = \oint_S \vec{D} \cdot d\vec{s} = Q_{\text{enclosed}} = \vec{G} \cdot \hat{n} \cdot S \quad \vec{D} = \frac{\Phi}{S} = \epsilon \cdot \vec{E}, \quad \epsilon = \epsilon_r \cdot \epsilon_0$$

Field
Normal of surface
Area of surface

Relative Permittivity

- Total flux through surface is equivalent to charge enclosed by surface
- A ball of charge can be treated as point charge
- Flux through any surface:

$$\Phi = \pm \iint_D \vec{G} \cdot \left(\frac{\partial \vec{r}}{\partial u} \times \frac{\partial \vec{r}}{\partial v} \right) dS = \iiint_V \nabla \cdot \vec{D} dV$$

parametrised domain
dual
charge density: ρ_v

$\hat{n} d\vec{r}(u,v)$
equals volume

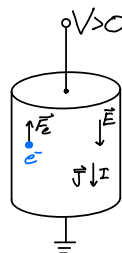
- Divergence can be used to determine flux through surface of volume V

Conductors

$$\vec{F}_e = -e \cdot \vec{E} \quad \text{diff velocity} \quad \vec{v}_d = -\mu_e \cdot \vec{E} \quad \text{mobility constant}$$

current density

$$\vec{J} = \rho_v \cdot \vec{v} = \rho_e \cdot \vec{v}_d = -\rho_e \cdot \mu_e \cdot \vec{E} = \sigma \cdot \vec{E} \quad \left[\frac{\text{Ampere}}{\text{m}^2} \right]$$

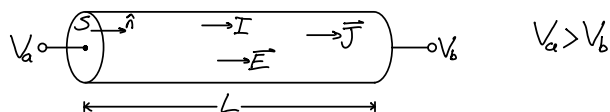


$$I = \iint_S \vec{J} \cdot d\vec{s} = \iint_S \vec{J} \cdot \hat{n} dS$$

$$V_{ab} = - \int_b^a \vec{E} \cdot \hat{n} dl = E \cdot L \rightarrow E = \frac{V_{ab}}{L}$$

$$V = \left\{ \frac{L}{\sigma S} \right\} \cdot I$$

$$\text{resistance} = R = \frac{- \int_a^b \vec{E} \cdot d\vec{l}}{\sigma \iint_S \vec{E} \cdot d\vec{s}}$$

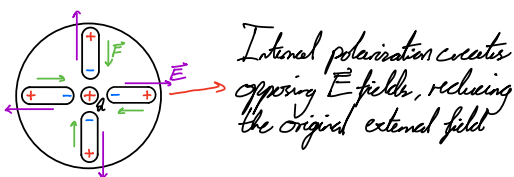
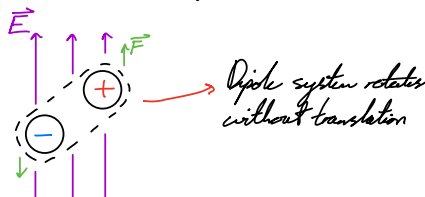


Dielectric

- Dipole: Two charges that are equal, opposite and close together

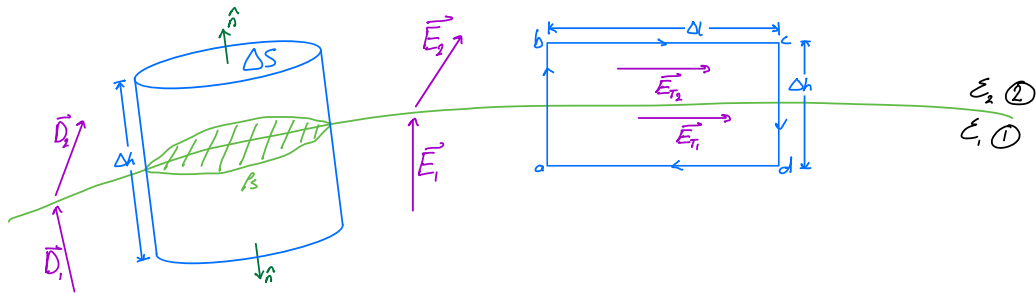
$$\vec{p} = q \cdot \vec{d}$$

electric dipole moment vector



Electric Boundary Conditions

- Electric field will reflect as it passes between dielectrics with different permittivities (ϵ)



Electric Field: $\lim_{\Delta h \rightarrow 0} (\oint \vec{E} \cdot d\vec{L}) = 0$

$$E_2 \cdot \Delta L - E_1 \cdot \Delta L = 0$$

$$E_2 = E_1$$

Flux Density: $\lim_{\Delta h \rightarrow 0} (\oint \vec{E} \cdot d\vec{L}) = Q_{enc}$

$$D_{N2} \Delta S - D_{N1} \Delta S = \rho_s \Delta S$$

$$D_{N2} - D_{N1} = \rho_s$$

- In a perfect dielectric (no free charge: $\rho_s = 0$) $\rightarrow D_{N2} = D_{N1} \rightarrow \epsilon_1 E_{N1} = \epsilon_2 E_{N2}$
- If one material is a conductor $\rightarrow D_{N2} = 0$; $D_{N1} = \rho_s$

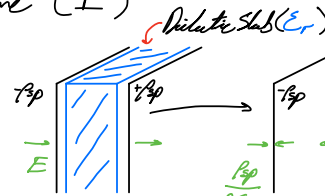
Polarization

- Number of dipole moments per unit volume ($\vec{P}$)

$$\vec{P} = \frac{\vec{P}}{V} = \frac{Qd}{sd} = \rho_{sp} \hat{d}$$

electric dipole moment vector

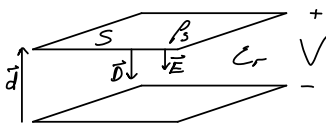
surface charge due to polarization



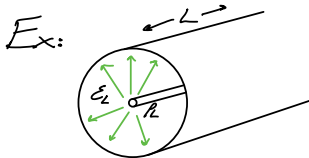
Model a dielectric as air

$$\vec{D} = \epsilon_0 \epsilon_r \vec{E}$$

Capacitance



$$C = \frac{|Q|}{|V|} = \frac{\int_S \rho_s ds}{\int_L \vec{E} \cdot d\vec{L}} = \frac{\epsilon \cdot S}{d} = \frac{\epsilon_r \cdot \epsilon_0 \cdot S}{d}$$



$$C = \frac{QL}{V} ; V = \int_{ring} \vec{E} \cdot d\vec{p} = \frac{P_L h(\frac{ring}{2\pi \epsilon_L \epsilon_0})}{2\pi \epsilon_L \epsilon_0} \rightarrow C = \frac{2\pi \epsilon_L \epsilon_0 L}{h(\frac{ring}{2\pi \epsilon_L \epsilon_0})}$$

- Two stacked dielectrics within plates behave like series, side-by-side behaves like parallel

Magnetostatics

Biot-Savart Law

- Relationship between current distribution and the field it generates

current filament $\vec{dl} = \frac{I d\vec{l} \times \hat{r}}{4\pi R^2}$

direction from filament to point

distance between filament to point

$\vec{B}$: Magnetic Flux Density [T]
 $\vec{H}$: Magnetic Field Intensity [A/m]
 μ_0 : Magnetic Permeability
 $4\pi \times 10^{-7}$

$H = \oint \frac{I d\vec{l} \times \hat{r}}{4\pi R^2} = \oint \frac{I dl \sin \theta}{4\pi R^2}$

angle between $\hat{r}$ & $d\vec{l}$

Ampere's Circuital Law

- Line integral of H about a closed path is equal to direct current enclosed by said path

$\oint \vec{H} \cdot d\vec{L} = I \longrightarrow \vec{\nabla} \times \vec{H} = \vec{J}$

current density at point of magnetic field

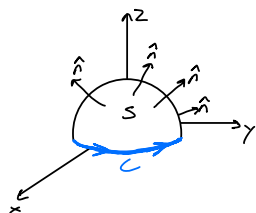
Magnetic Flux [Wb]

$\Phi = \iint_S \vec{B} \cdot d\vec{S} \longrightarrow \oint \vec{B} \cdot d\vec{S} = 0 \longrightarrow \vec{\nabla} \cdot \vec{B} = 0; (\vec{B} = \mu \vec{H}) \left[\frac{Wb}{m^2} \right]$

$\mu = \mu_0$

Stoke's Theorem

- Let "S" be a smooth surface that is bounded by a simple curve "C", then:



$\oint_C \vec{F} \cdot d\vec{r} = \iint_S \vec{\nabla} \times \vec{F} \cdot d\vec{S}$

Continuity of Current

$I = -\frac{d}{dt} Q_{enc} = \oint \vec{J} \cdot d\vec{S} = -\frac{d}{dt} \iiint_V \rho dV = \iiint_V \vec{\nabla} \cdot \vec{J} dV$

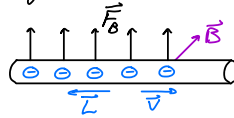
$\longrightarrow \vec{\nabla} \cdot \vec{J} = -\frac{d}{dt} \rho$

- Describes how charge enters/exits a system

Magnetic Forces/Torques

- Steady magnetic force is produced by moving charges $\rightarrow$ current

$$\vec{F}_B = d\vec{v} \times \vec{B} = i \vec{L} \times \vec{B}$$



- Torque on current loop
 - Current (I) encloses area (S) with normal ($\hat{n}$);
 - Magnetic Dipole Moment: $\vec{\mu}_m = NIS \cdot \hat{n}$

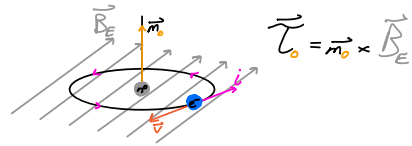
$$\vec{\tau}_B = \vec{\mu}_m \times \vec{B}$$

of turns current

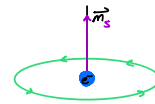
$$d\vec{\tau}_B = I d\vec{S} \times \vec{B}$$

Magnetic Materials

- Electrons orbiting the nucleus creates magnetic dipoles ($\vec{m}_o$)
- External field lines ($\vec{B}_E$) produce torque ($\vec{\tau}_o$) on the system



- Electron spin generates magnetic dipole moments
 - Simplified and approximated value of $9.28E-24 [A \cdot m^2]$



- Diamagnetic
 - Magnetic moments produced by the spin and the orbit of the electrons cancel out: $\vec{m}_s + \vec{m}_o = 0 \rightarrow$ external fields ($\vec{B}_E$) do not produce torque
 - External fields are repelled by diamagnets $\rightarrow \vec{B}_{in} < \vec{B}_{out}$

- Paramagnetic
 - $\vec{m}_s + \vec{m}_o \neq 0 \rightarrow \vec{B}_E \neq 0$
 - When an external field is applied paramagnetic dipoles align to enhance external fields $\rightarrow \vec{B}_{in} > \vec{B}_{out}$

- Ferromagnetic
 - Large atomic moments caused by greater electron spin $\rightarrow \vec{m}_s \gg \vec{m}_o$
 - Domain: regions of atomic dipoles that are all magnetically aligned
 - Overall moment of ferromagnet is 0, unless it has been exposed to an external field before
 - When exposed to $\vec{B}_E$; some domains align increasing $\vec{B}_{in}$ to be much larger than $\vec{B}_{out}$
 - Hysteresis: newly aligned dipoles do not return to original alignment in absence of $\vec{B}_E$
 - Curie Temperature: above this temperature ($570^\circ C$) ferromagnets revert to paramagnets
 - Soft Ferromagnets: easy to magnetize/demagnetize
 - Hard Ferromagnets: hard to magnetize/demagnetize

Magnetization

- Magnetic Dipole Moment due to single orbiting electron:
- Sum of Dipoles (n) is volume (ΔV) is $\vec{M}$

$$\vec{M} = \lim_{\Delta V \rightarrow 0} \frac{1}{\Delta V} \sum_{i=1}^{n \Delta V} \vec{\mu}_{m_i} \rightarrow i_B = \oint \vec{M} \cdot d\vec{L}$$

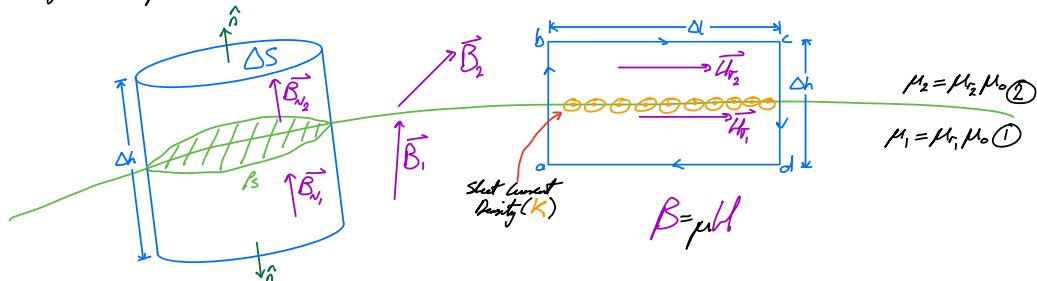
$$\vec{\mu}_m = i_B d\vec{S}$$

band current surface area of electron's path

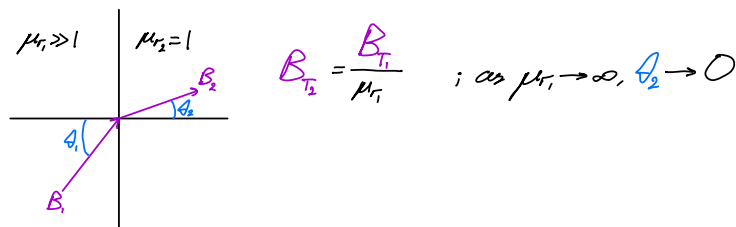
- Total current (i_r) through closed loop: $i_r = \oint (\frac{\vec{B}}{\mu_0} - \vec{M}) \cdot d\vec{L} \rightarrow \vec{B} = \mu_0 (\vec{H} + \vec{M})$
- " $\vec{M}$ " is zero in free space
- Magnetic Susceptibility (χ_m): $\mu_r = 1 + \chi_m$; $\vec{M} = \chi_m \vec{H} \rightarrow \vec{B} = \mu_r \mu_0 \vec{H}$

Magnetic Boundary Conditions

- Magnetic field

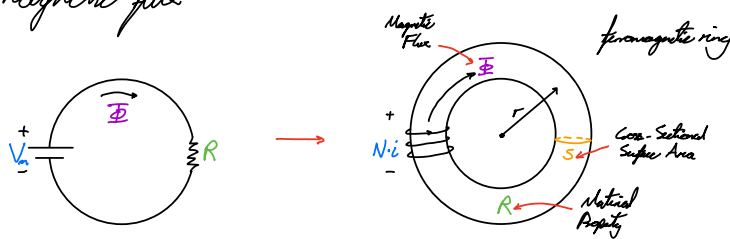


- Normal component of magnetic field is continuous: $B_{1n} = B_{2n}$
- Tangential component: $\mu_1 H_{1t} - \mu_2 H_{2t} = K$
 - $K = 0 \rightarrow \mu_2 B_{1t} = \mu_1 B_{2t}$
- If material has much higher permeability than medium, the incidence field angle approaches 0



Magnetic Circuits

- A magnetic circuit is made up of one or more closed loop paths containing magnetic flux



- Magnetomotive Force ($V_m = Ni$) [Amp-Turns]
 - Wrap current carrying coil around magnetically permeable material
 - Insert permanent magnet into ring
- Reluctance (R) [$1/H$]
 - Flow of flux around magnetic circuit is resisted by reluctance of magnetic circuit

$$R = \frac{L}{\mu S}$$

$\leftarrow$ length of material
 $\leftarrow$ Magnetic Permeability

- Flux flows through path of least reluctance

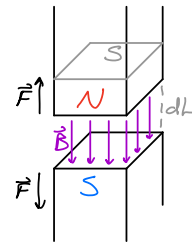
- Magnetic Flux (Φ) [Wb]
- Ohm's Law applied to magnetostatics: $V_m = \Phi \cdot R$

Magnetic Potential Energy

$$W_m = \frac{1}{2} \iiint \vec{B} \cdot \vec{H} dV = \frac{1}{2} \iiint \frac{B^2}{\mu} dV$$

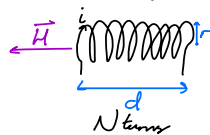
- Applies to magnetically linear mediums such as air
- Magnetically opposed poles have an attractive force between them
- Consider the work done to separate the poles:

$$dW_m = F dL = \frac{B^2 S dL}{2\mu_0} \rightarrow F = \frac{B^2 S}{2\mu_0}$$



Solenoids

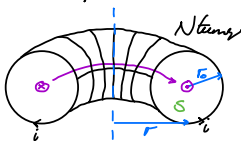
- Coil of wire used as an electromagnet
- Concentrates the magnetic field down center of coil



$$H = \frac{N \cdot i}{d} \left[\frac{A}{m} \right]$$

Toroids

- Donut-shaped coil of wire used as an electromagnet



$$H = \frac{N \cdot i}{2\pi r} \left[\frac{A}{m} \right]$$

Inductors

- Device for storing energy in a magnetic field
- Creates magnetic flux lines which form closed loops
 - These lines may also pass through other coils

- Self-Inductance is the ratio of total flux linkage to the linked current: $L = \frac{N\Phi}{i}$

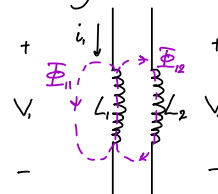
Mutual Inductance

- Change in magnetic flux may result from nearby coil
- The ability of one inductor to induce a voltage across a nearby inductor

$$\Phi_1 = \Phi_{11} + \Phi_{12}$$

$$V_1 = N_1 \frac{d\Phi_1}{dt} \quad V_2 = N_2 \frac{d\Phi_{12}}{dt} = M_{21} \frac{di_1}{dt}$$

$$M_{21} = N_2 \frac{d\Phi_{12}}{di_1} = N_2 \frac{\Phi_{12}}{i_1} [H]$$



- Physical Inductance: $L = \mu \frac{N^2 S}{l}$
 cross section of inductor
 length of inductor
- Energy: $W_H = \frac{L i^2}{2}$

- Energy Conservation bounds Mutual-Inductance

$$M \leq \sqrt{L_1 L_2} \rightarrow K = \frac{M}{\sqrt{L_1 L_2}} = \frac{\Phi_{12}}{\Phi_{11} + \Phi_{12}} ; \quad 0 \leq K \leq 1$$

No magnetic flux crossover
 Maximum magnetic flux crossover

- K is a measure of how much magnetic flux passes from one coil to the other

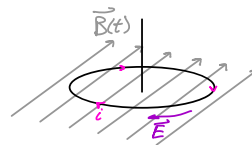
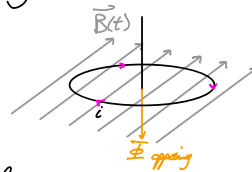
Induced Electromotive Forces (Faraday's Law)

$$\text{emf} = -N \frac{d\Phi}{dt} [\text{Volts}] = -N \frac{d}{dt} \int_S \vec{B}(t) \cdot d\vec{S}$$

- emf can be produced by:
 - 1) Change in $B(t)$
 - 2) Change in surface that flux is passing through
 - 3) Change in B with location

$$\text{emf} = \oint_L \vec{E} \cdot d\vec{l} \neq 0$$

Not zero in time-varying case

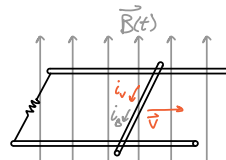


- stationary loop in time-varying B field results in:

$$\vec{\nabla} \times \vec{E} = - \frac{d\vec{B}(t)}{dt}$$

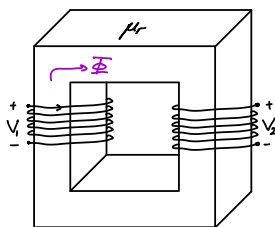
- moving conductor in time-varying B field results in:

$$\begin{aligned} \vec{\nabla} \times \vec{E} &= \vec{\nabla} \times \vec{E} + \vec{\nabla} \times \vec{E} \\ &= - \frac{d\vec{B}(t)}{dt} + \vec{\nabla} \times (\vec{v} \times \vec{B}) \end{aligned}$$



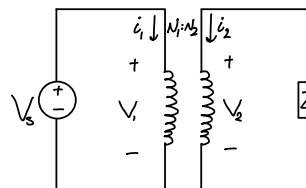
Transformer

- Step-Up transformer: $V_2 > V_1$; $i_2 < i_1$
- Step-Down transformer: $V_2 < V_1$; $i_2 > i_1$



$$V_1 = N_1 \frac{d\Phi}{dt}$$

$$V_2 = N_2 \frac{d\Phi}{dt}$$

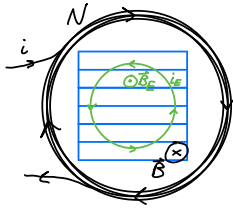


$$\frac{V_2}{V_1} = \frac{N_2}{N_1}$$

$$\frac{i_2}{i_1} = - \frac{N_1}{N_2}$$

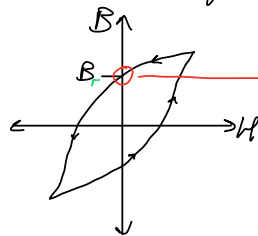
- At steady state, the emf and Φ in core are same as before load was connected

- Eddy Currents
 - Loops of current induced within conductors by a changing $\vec{B}$ field



$\vec{B}_E$ is induced by $\vec{B} \rightarrow$ generates Power loss: $P_L = i_E^2 \cdot R$

- Sheets of ferromagnets that are insulated from each other prevent Eddy Currents
- Hysteresis: Magnetic Flux Density lags behind Magnetic Field Intensity
 - Newly realigned dipoles do not all return to their previous arbitrary directions
 - Hysteresis loop: The relationship between B & H as material is magnetized and demagnetized repeatedly



even when the magnetic field intensity (H) is 0, there is still residual flux density (B_r)

- Hysteresis Loss: Every cycle of the Loop results in energy lost to heat due to the friction generated from dipole movement

Displacement Current (I_d)

- Displacement current density ($\vec{J}_d$) is the result of time-varying electric flux density ($\frac{d\vec{D}}{dt}$)
- Ampere's Circuital Law becomes:

$$\vec{\nabla} \times \vec{H} = \vec{J} + \vec{J}_d$$

$$I_d = \iint_S \frac{d\vec{D}}{dt} \cdot d\vec{S}$$

$$\oint \vec{H} \cdot d\vec{L} = I + I_d$$

Maxwell's Equations

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \times \vec{H} = \vec{J} + \frac{d\vec{D}}{dt}$$

$$\vec{\nabla} \cdot \vec{D} = \rho$$

$$\vec{\nabla} \cdot \vec{B} = 0$$